Fabrication and Characterization of Polysulfone-Zeolite ZSM-5 Mixed Matrix Membrane for Heavy Metal Ion Removal Application

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ABSTRACT

Mixed matrix membranes (MMMs) of Polysulfone (PSf)-Zeolite ZSM-5 (ZZSM-5) were prepared by phase inversion method with a dose ranging from 1.0 to 4.0 Wt. % with polyvinylpyrrolidone (PVP) as the fore forming agent. The prepared mixed matrix membranes were scrutinized for their permeation, hydrophilicity and anti-fouling nature. Characterization of the membrane was carried out by Electrokinetic analyzer. The heavy metal ions rejection experiment has been carried out and the results manifested that, the PZM-4 membrane exhibits higher pure water flux of 348.88 L/m² h, contact angle of 72.7° and the heavy meals rejection of Pb²⁺ (98.54%) and of Cd²⁺ (95.32%) ions. Taken as a whole, the modified PSf-ZZSM-5 ultrafiltration membranes are the attractive candidate for the water treatment.

Keywords: Polymers, Zeolite ZSM-5, Polysulfone, Membranes, Heavy metal rejection, Hydrophilic additive

1.0 INTRODUCTION

omnipresent The most problem distressing human across the globe is insufficient potable water. Adopting these glitches calls out for the water purification. In the forthcoming decades, there will be an intensification of potable water demand even in the water abundant regions [1]. Water scarcity hails from prompt development and industrialization. Contaminant such as heavy metal ions have led to severe environmental concerns [2]. Membrane filtration is one of the ways out to get rid of water contamination since it encompasses low energy consumption, no phase change, easy scale-up and maintenance [3, 4]. Membrane properties are flexible and pore size can be adaptable according to their applications [5]. Membrane technology is broadly pertinent in many areas such as dye removal, desalination and heavy metal rejection [6, 7, 8].

Detrimental heavy metal such as cadmium, nickel. zinc. copper. mercury, chromium. and lead contamination of the environment is a weighty universal glitch [9]. Principally, lead (Pb) poisoning i.e. plumbism is one of the major issues as it affects the human body segments such as heart, bones, intestines, kidneys, and reproductive and nervous systems. The entry of lead into the human body can cause symptoms like abdominal pain, confusion, headache,

anemia, irritability, and in severe cases seizures. coma, and death [10]. Recently FDA warns of Pb poisoning risk from cosmetic clay. Moreover, lead has no known useful role in living World organism [11]. Health Organization (WHO) has established maximum contaminant the level (MCL) of Pb in drinking water at 15µg/L [12]. In addition, cadmium (Cd) has been recognized as very toxic and it has been merged in "Big Three" category of heavy metals [13]. Symptoms of acute poisoning include headaches. nausea. vomiting, weakness, pulmonary edema and diarrhea and a disease called "Itai-Itai" in Japan is specifically associated with cadmium poisoning [14]. From the above fallouts, it is much exculpated that we need a confiscated system to get rid of heavy metal toxicity. Mixed matrix membranes would be the spot-on alternative to fulfill the above-mentioned requirements with the uniform distribution zeolite of ZSM-5 throughout the membrane matrix. They furnish better separation properties to membranes because of their adapted permeability, worthy selectivity, mechanical strength, thermal stability chemical resistance and [15]. Polysulfone (PSf) based membranes are rummage-sale as ultrafiltration and microfiltration system most extensively for its outstanding heat resistance, chemical compatibility and durable over a wide range of pH [16]. The major drawback of these PSf membranes is that they are hydrophobic in nature. However the water purification membranes necessitate substantial hydrophilicity in order to cope up with productivity issues. Similarly, membranes suffer from fouling and hence lead to low membrane lifetime [17]. The low permeability and fouling are predominantly due to low surface hydrophilicity and low porosity. So, all over the globe, researchers are looking for a membrane with finely-balanced characteristics. As per the literature is concerned, adding the hydrophilic additive to PSf membrane can increase the hydrophilicity, permeability and antifouling property [18]. Kumar et al. investigated the effect of adding Nsuccinyl chitosan as an additive to PSf membrane. The modified PSf membrane exhibited enhanced hydrophilicity and permeation fluxes with flux recovery ratio of 70% the compared to pristine PSf [19]. Moideen et al. membrane reported the effect of adding poly (ethylene glycol) 1,000 (PEG) on the morphology and membrane properties. The results have shown that permeability, hydrophilicity, and antifouling property have been augmented. Also, the tailored membrane has shown flux recovery ratio of 72.84% and the heavy metal such as Pb^{2+} and Cd^{2+} rejection of 99.48 and 95.5% [20]. Ana et al. studied the effect of polyvinylpyrrolidone the on morphology and membrane properties. The improved pore density and membrane permeability were observed for the modified membrane than the virgin membrane [21]. Kumar et al. investigated more extensively the influence of poly (N-vinylcaprolactamco-acrylic acid) as an additive to PSf membrane. The pure water flux increased from 1 to 18.8L/m²h, water contact angle decreased from 76° to 58°, an increase in BSA flux and decrease in membrane fouling was observed [22]. Yilmaz et al. described impregnation the of zeolite nanoparticles to PSf membrane and the modified membrane exhibited good heavy metal adsorption [23]. Leixi et al. prepared the PSf membrane embedded with Linda type zeolite nanoparticle which manifested

resistance to hydraulic shear detachment, enhanced hydrophilicity with water contact angle reduced from 66° to 40° and anti-biofouling ability [24]. Fu *et al.* incorporated the zeolites 4A into PSf membrane and confirmed the enrichment of pure water flux, rejection, thermal and mechanical stability [25]. From the above results, it can be ascertained that adding the hydrophilic additive would improve the PSf membrane filtration properties.

However, the use of zeolite ZSM-5 (see Figure 1) has not yet been reported as the hydrophilic additive to polymeric materials. In the present study, well-dispersed zeolite ZSM-5 has been used as a hydrophilic additive to modify PSf membrane. The PSf-ZZSM-5 mixed matrix membranes were prepared by diffusion induced phase separation method with different amounts of additive dosage ranging from 1.0 to 4.0 wt. %. Pore-forming agent polyvinylpyrrolidone (PVP) was used and the effect of the hydrophilic additive on the membrane surface structure and performance were scrutinized in detail. Dynamic water contact angle measurement was used to the membrane depict surface hydrophilicity. The surface charge of the membrane has been studied by using Electrokinetic analyzer. The performance modified of the membranes was studied in terms of water uptake capacity, water flux, and membrane hydraulic resistance. Additionally, antifouling and heavy metal ion rejection behavior were reconnoitered in detail.



Figure 1 Topology of ZZSM-5

2.0 METHODS

2.1 Materials

PSF (Mw 35,000), (PVP) Polyvinylpyrrolidone were purchased from Sigma-Aldrich Co., India. ZZSM-5 was a gift sample from King Fahd University for Petroleum & Minerals, Saudi Arabia. N-methyl-2pyrrolidone (NMP) was purchased from Merck India, Ltd. Bovine serum albumin (BSA) (Mw ~ 69 kDa) was purchased from CDH Chemicals, India. Polyethyleneimine (PEI) (Mw ~ 60,000) was purchased from Acros Organics, USA. Cadmium nitrate tetrahydrate and lead nitrate were purchased from Sigma-Aldrich Co., India.

2.2 Preparation of Membranes

PSf-ZZSM-5 mixed matrix membranes were prepared by phase inversion method [8]. The calculated amount of ZZSM-5 (0 wt. % to 4 wt. % of PSf dosage) was dispersed in a suitable volume of NMP and sonicated for 15 temperature. min at room The anticipated quantity of PSf (overall 20 wt. % of the polymer concentration of the final casting solution) was added to the above dispersed solution along with 2 wt. % of the invariable pore forming agent PVP and the solution was stirred for 24 h at 50 °C to obtain a homogeneous casting solution. The obtained solution was kept for an hour without stirring at the similar temperature to discard imprisoned air. The casting solution was spread on a clean glass plate and cast using a doctor's blade. Then it was immersed into a water bath and allowed to stand in a coagulation bath for 24 h to comprehensive confirm phase inversion. Α summary of the compositions of the membranes is given in Table 1.

Membrane code	PSf(g)	NMP (g)	ZZSM- 5 (g)	PVP (%)	
PZM-0	18	80	0	2	
PZM-1	18	79.8	0.18	2	
PZM-2	18	79.6	0.36	2	
PZM-3	18	79.4	0.54	2	
PZM-4	18	79.2	0.72	2	

Table 1 Casting solution composition

 $^aW_{ZZSM\text{-}5}$ is the mass ratio of ZZSM-5 to PSf

2.3 Electrokinetic Analysis

Zeta-potential of the membranes surface was determined by a streaming current electro kinetic analyzer (SurPass, Anton Paae GmbH, Graz, Austria). The flow channel gap was set at 100 mm, and a 1 mM KCl solution at 20 °C was used as the background electrolyte. Streaming current was determined in a pH range of 2-10, adjusted using HCl and NaOH. Membrane zeta potential (ζ) was using the Helmholtzcalculated Smoluchowski equ (1)

$$\zeta = \frac{dI}{dp} \frac{\mu}{\epsilon \epsilon_0} \frac{L}{A} \tag{1}$$

where dI/dp is the slope of the streaming current versus pressure, μ is the solution dynamic viscosity, ε is the dielectric constant of the solution, ε_o is the vacuum permittivity, L is the streaming channel length and A is the cross-section of the streaming channel. Figure 2 is the schematic representation of the adjustable gap cell.





Figure 2 Vision along the streaming channel inside the adjustable-gap cell (top) and schematic representation of membrane mounting inside the adjustable-gap cell; right: cross section of samples holders [27]

2.4 Water Uptake and Contact Angle Measurement

The water uptake capacity of the membrane is a significant factor to govern its hydrophilicity. The dry membranes were cut into 2 cm² sized pieces and weighed. These membrane samples were soaked in distilled water for 24 h and weighed after smearing with blotting paper followed by the wet membranes were dried under vacuum at 70 °C for 24 h. The dry weights were determined and the percentage water content in the membrane was calculated using eqn (2)

$$\text{\%uptake} = \left(\frac{W_w - W_d}{W_w}\right) \times 100 \tag{2}$$

where W_w and W_d are the weight of wet and dry membrane samples respectively.

The change in the hydrophilicity of the prepared membranes after adding

the ZZSM-5 was confirmed by measuring the water contact angle (WCA). The surface hydrophilicity was measured by an FTA-200 Dynamic contact angle analyzer using the sessile droplet method. In order to minimize the experimental errors, the WCA measurement of each sample was measured three times and the average value was reported.

2.5 Pure Water Flux Study

The pure water flux (PWF) of the membranes were determined using dead end filtration unit at room temperature. Membrane area of 5 cm^2 was dipped in Deionized water for 24h before commencing the filtration. The setup was aided with a nitrogen cylinder as the pressure source. Each membrane was compacted at 5 bar pressure for 30 min before beginning the experiment. After compacting, deionized water was passed through the membrane for 80 min at 4 bar pressure to acquire PWF J_w (L/ m² h). The flux was calculated using the formula (3) and Figure 3 is the schematic illustration of the lab scale filtration arrangement.

$$J_w = \frac{Q}{\Delta tA} \tag{3}$$

where, J_w is PWF and 'Q' is the amount of water collected for Δt (h) time duration using a membrane of area 'A' (m²).



Figure 3 Schematic illustration of the lab scale filtration arrangement

2.6 Antifouling Properties

The membrane fouling behavior was examined using the reported literature [28]. In brief, the pure water flux of the membrane J_{w1} (L/(m² h)) was tested at 4 bar transmembrane pressure (TMP). Then, 0.8 g/L bovine serum albumin (BSA) aqueous solution was fed into the ultrafiltration system followed by the filtration of BSA for 80 minutes. The flux for BSA solution measured based on the quantity of water permeating the membranes is J_p $(L/m^2/h)$. The membrane was flushed with pure water for 10 minutes and then pure water flux of the membrane J_{w2} (L/(m² h)) was calculated. The flux recovery ratio (FRR) was calculated using Eq. (4) to assess the membrane antifouling property.

$$FRR(\%) = \frac{J_{W2}}{J_{W1}} \times 100$$
 (4)

The membrane fouling was further assessed by calculating the reversible R_{rev} and irreversible R_{irr} fouling ratio by following equation (5) and (6)

$$R_{rev}(\%) = \frac{J_{w2} - J_p}{J_{w1}} \times 100$$
 (5)

$$R_{\rm irr}(\%) = \frac{J_{w1} - J_{w2}}{J_{w1}} \times 100 \tag{6}$$

2.7 Heavy Metal Rejection Study

The experiment was executed as per the literature procedure [8]. In brief, an aqueous solution of lead nitrate and cadmium nitrate was prepared in the presence of 1 wt. % of polyethyleneimine with an initial concentration of 1000 ppm. The pH of the subsequent solution was adjusted to 6 ±0.5 using 0.1 M HCl or 0.1 M NaOH solution. The attained solution was stirred for 5 days at room temperature to persuade complex formation. The heavy metal ions rejected by the membranes were determined by calculating the metal ion concentration in the feed and permeate using an AAS (atomic absorption spectrometer). The percentage of metal ions rejected by the membranes were calculated using the eqn (7)

$$\% R = \left(1 - \frac{c_p}{c_f}\right) \times 100 \tag{7}$$

where C_p and C_f are the concentrations of heavy metal ions in the permeate and feed respectively.

3.0 RESULTS AND DISCUSSION

3.1 Electrokinetic Analysis

Zeta potential measurements for the pure PSf and modified membrane is shown in Figure 4. The modified membrane has hydroxyl and sulfone group which will be protonated at low pH leading to positive zeta potential value. Moreover at high pH the groups will be deprotonated causing negative zeta potential value. The modified membrane manifested higher zeta potential value (-43 mV) than the pure PSf membrane (-34 mV) due to the presence of ZSM-5 on the membrane surfaces. Evidently, the addition of ZSM-5 has capacity for improving the separation efficacy of pure PSf membrane since hydrophilicity and anti-fouling proficiency increase as the membrane surfaces become more hydrophilic, energetic and charged [29]. Figure 4 represents the zeta potential values.



Figure 4 Zeta potential value of PZM-O and PZM-4

3.2 Water Uptake Capacity and Contact Angle

hydrophilic The nature of the membrane can be ascertained by measuring their water uptake capacity and contact angle. The water uptake capacity of the membrane depends on number of hydrophilic sites and the existence of macrovoids in the membrane [7]. The water uptake capacity of all the membranes is presented in Figure 5. The PZM-0 membrane has shown the water uptake capacity of 58.5% and it has been increased as ZSM-5 content increased.

The increase in water uptake capacity designates the increased hydrophilic sites and the increased macro voids in the membranes.

In general contact angle is the measure of surface hydrophilicity of the membrane, smaller the contact angle greater the hydrophilicity and Moreover vice versa. PZM-4 membrane has shown the contact angle of 72.7°. Since the contact of pristine PZM-0 membrane was 79.9°, the ZSM-5 could have addition of increased the hydrophilicity (Figure 5) of the membrane. The values are tabulated in Table 2.



Figure 5 Water uptake capacity and contact angle of the membrane

Membrane code	Contact angle (°)	Pure water flux (L/m² h)
PZM-0	79.9	55.9119
PZM-1	78.6	101.5119
PZM-2	77.8	239.1382
PZM-3	75.6	291.9382
PZM-4	72.7	348.88

Table 2 Properties of the prepared membranes

3.3 Pure Water Flux

Filtration experiment has been done to demonstrate the pure water flux (PWF) of the modified membrane. The PWF values are tabulated in Table 3. Here, the hydrophilicity is one of the prime factor which decides the permeation of water through the membrane. Figure 6 represents the PWF of the membrane. The PZM-0 membrane bared minimum flux of 81.13 L/m² h whereas the PZM-4 membrane uncovered maximum flux of 393.02 L/m^2 h. The augmentation of flux can be attributed to the addition of hydrophilic additive ZZSM-5, as a result hydrophilicty of the membrane upsurges and the contact angle of the modified membrane diminutions than the pristine membrane. In addition, the zeolite ZSM-5 microphorous is alumino silicates, which could be the supplementary reason for the increment of hydrophilicity. As a result ZZSM-5 would be good hydrophilic stuff.

	Permeate flux (L/m ² h)			FRR and fouling performance (%)			
Membrane code	\mathbf{J}_{w1}	\mathbf{J}_{p}	\mathbf{J}_{w2}	FRR	Rt	Rr	R _{ir}
PZM-0	55.9119	3.45	15.3415	27.4387	93.82	21.26	72.56
PZM-1	101.5119	20.55	44.98045	44.31052	79.75	24.06	55.68
PZM-2	239.1382	46.53	151.7367	63.45148	80.54	43.99	36.
PZM-3	291.9382	50.23	195.5446	66.9815	82.79	49.77	33.01
PZM-4	348.8834	54.13	251.1118	71.97585	84.48	56.46	28.02

Table 3 Filtration and antifouling performance of the membrane



Figure 6 Time depentent pure water flux of the membrane

3.4 Antifouling Performance of the Membrane

It has been well documented that, all pressure driven processes are bound to

foul. It may lead to the decline of membrane performance. Fouling is caused by the deposition or adsorption of particles, proteins, colloids, salts, macromolecules, etc., on the membrane surface or inside the pores [30]. As a result, the flux in the course of BSA rejection falloffs considerably compared to the pure water flux [28]. In addition, surface hydrophilicity plays a major role in fouling. Figure 7 shows the flux of the modified and unmodified membranes at 4 bar pressure at 28 °C in altered environments i.e. before **BSA** filtration, during BSA filtration and after BSA filtration. There was a decline in flux during BSA rejection on account of the adsorption or deposition of protein molecules on the membrane surface, which affects the hydrophilicity of the membrane as well. The prepared membranes are hydrophilic in nature so they have exhibited lower attraction on the way to protein binding. In order to examine the antifouling property, calculation of flux recovery ratio is the spot-on fouling method [31]. The total performance and flux recovery ratio (FRR) are tabulated in Table 4. The pristine membrane PZM-0 unveiled FRR of 27.43% and fouling ratio (Rt) of 93.82% in consequence of the hydrophobic nature. The membrane PZM-4 exhibited FRR of 71.97% owing to the increased hydrophilicity by adding ZZSM-5. So the foulant could be removed by simple hydraulic cleaning. Therefore the membrane is having ample reversible nature. In addition, based on the FRR and total performance fouling it can be ascertained that the prepared membrane is having better antifouling properties and the obtained results are quite comparable with hydrophilic additives such as graphene oxide, silica and TiO₂ nanoparticles [32, 33, 34, 35].

3.5 Heavy Metal Ion Rejection Study

Heavy metal ions are toxic to human health and lead to the environmental pollution [15]. Since heavy metals are non-biodegradable one has to take prime action to control the heavy metal pollution. In the present study, rejection study of PSf and modified PSf have been demonstrated for Pb^{2+} and Cd^{2+} ions and presented in Figure 8.



Figure 7 Flux against time for membranes at 4 bar pressure under three conditions: water flux for 80 min, 0.8 g L^{-1} BSA solution flux for 80 min, and water flux for 80 min after detailed washing with distilled water



Figure 8 The heavy metal ions rejection of modified membranes

The membrane PZM-4 publicized the rejection of Pb^{2+} and Cd^{2+} ionswere 98.56 and 95.32% respectively.

PZM-0 exhibited Moreover the rejection of Pb^{2+} and Cd^{2+} ions were 33.4 and 27.2% respectively. It is evident from the results that as the concentration of ZZSM-5 increases the rejection ability also increases. This is because, the PSf membrane is hydrophobic nature. in SO the interaction between the heavy metal ions and the membrane is considerably ZZSM-5 less. Bv adding as hydrophilic additive, it increases the hydrophilicity of the modified membrane. The complexation capacity of the metal ions with polyethyleneimine (PEI) depends on the size of metal ion i.e. bigger Pb²⁺ ions complexes more effectively than the Cd^{2+} ions. As a result the bigger Pb²⁺ ions are rejected greater than the smaller Cd²⁺ ions [20]. The order of heavy metal rejection is $Pb^{2+} > Cd^{2+}$ ions. It can also be comprehended that while complexing with PEI the size of metal ion increases since it forms metal complex [8].

4.0 CONCLUSION

The mixed matrix membranes were prepared by phase inversion method with different amount of ZSM-5 (0 to 4 wt. %). The results have been revealed that the modified membranes exhibited improved pure water flux. hydrophilicity and water uptake capacity. In addition the membrane PZM-4 has shown FRR of 71.9% and reversible fouling of reversible fouling ratio of 56.4%. Correspondingly, the modified membrane has ability to adsorb heavy metal ions such as Pb²⁺ and Cd^{2+} ions. Overall, the ZSM-5 is the effective hydrophilic additive for improving the performance of the membrane.

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REFERENCES

- M. A. Shannon, P. W. Bohn, M. Elimelech, J. G. Georgiadis, B. J. Marinas and A. M. Mayes. 2008. Science And Technology For Water Purification In The Coming Decades. *Nature*. 452: 301–310.
- [2] H. W. Liang, X. Cao, W. J. Zhang, H. T. Lin, F. Zhou, L. F. Chen and S. H. Yu. 2011. Robust and Highly Efficient Free-Standing Carbonaceous Nanofiber Membranes for Water Purification. Adv. Funct. Mater. 21: 3851–3858.
- J. Yin and B. Deng. 2015.
 Polymer-Matrix Nanocomposite Membranes For Water Treatment. J. Membr. Sci. 479: 256–275.
- [4] Anna Lee, Jeffrey W. Elamb and Seth B. 2016. Darling, Membrane Materials For Water Purification: Design, Development, And Application Environ. Sci. Water Res. Technol. 2: 17–42.
- [5] N. C. van de Merbel, J. J. Hageman, U.A. Th. Brinkman. 1993. Membrane-based Sample Preparation For Chromatography. J. Chromatogr. 634: 1–29.
- [6] Valeen Rashmi Pereira, Arun M. Isloor, Udaya K. Bhat, A. F. Ismail, Abdulrahman Obaid and Hoong-Kun Fun. 2015. Preparation And Performance Studies Of Polysulfone-Sulfated Nano-Titania (S-Tio2) Nanofiltration Membranes For Dye Removal. *RSC Adv.* 5: 53874.

- B. M. Ganesh, Arun M. Isloor,
 A. F. Ismail. 2013. Enhanced Hydrophilicity And Salt Rejection Study Of Graphene Oxide-Polysulfone Mixed Matrix Membrane. *Desalination*. 313: 199–207.
- [8] Raghavendra S. Hebbar, Arun M. Isloor, K. Anandab and A. F. Ismail. 2016. Fabrication Of Polydopamine Functionalized Halloysite Nanotube/Polyetherimide Membranes For Heavy Metal Removal. J. Mater. Chem. A. 4: 764–774.
- [9] Hyun Gyu Park, Tae Won Kim, Myeong Yun Chae, Ik-Keun Yoo. 2007. Activated Carbon Containing Alginate Adsorbent For The Simultaneous Removal Of Heavy Metals And Toxic Organics. *Process Biochemistry*. 42: 1371–1377.
- [10] N. Abdullah, R. J. Gohari, N. Yusof, A. F. Ismail, J. Juhana, W. J. Lau, T. Matsuura. 2016. Polysulfone/Hydrous Ferric Oxide Ultrafiltration Mixed Matrix Membrane: Preparation, Characterization And Its Adsorptive Removal Of Lead (II) Aqueous From Solution. Chemical Engineering Journal. 289: 28-37.
- [11] E. Ayranci, O. Duman. 2004. Binding Of Lead Ion On Bovine Serum Albumin Studies By Ion Selective Electrode. *Protein Pept. Lett.* 11: 331–337.
- [12] R. Jamshidi Gohari, W. J. Lau, T. Matsuura, E. Halakoo, A. F. Ismail. 2013. Adsorptive Removal Of Pb (II) From Aqueous Solution By Novel PES/HMO Ultrafiltration Mixed Matrix Membrane. Sep. Purif. Technol. 120: 59–68.

- [13] B.Volesky. 2007.Biosorption And Me. Water Res. 41: 4017– 4029.
- T. Theophanides, J. 2002.
 Anastassopoulou, Copper and Carcinogenesis. *Crit. Rev. Oncol. Haematol.* 42: 57–64.
- [15] Xiaoqin Zou, Guangshan Zhu, Hailing Guo, Xiaofei Jing, Diou Xu, Shilun Qiu. 2009. Effective Heavy Metal Removal Through Porous Stainless- Steel-Net Supported Low Siliceous Zeolite ZSM-5 Membrane. *Microporous and Mesoporous Materials*. 124: 70–75.
- [16] M. Mulder. 1996. Basic Principles of Membrane Technology. Second edition. Kluwer Academic Publishers.
- [17] Dong, Y. Y. Xu, Z. Yi, J. L. Shi.
 2009. Modification Of Polysulfone Membranes Via Surface-Initiated Atom Transfer Radical Polymerization. *Appl.Surf.Sci.* 255: 8860–8866.
- [18] Raghavendra S. Hebbar, Arun M. Isloor, A. F. Ismail, Simon J. Shilton, Abdulrahman Obaid and Hoong-Kun Fun. 2015. Probing The Morphology And Anti-Organic Fouling Behavior Of A Polyetherimide Membrane Modified With Hydrophilic Organic Acids As Additives. *New J. Chem.* 39: 6141–6150.
- [19] Rajesha Kumar, Arun M. Isloor, A. F. Ismail, T. Matsuura. 2013. Performance Improvement Of Polysulfone Ultrafiltration Membrane Using N-Succinyl Chitosan As Additive. *Desalination.* 318: 1–8.
- [20] Irfana Moideen K, Arun M. Isloor, A. F. Ismail, Abdulrahman Obai Hoong-Kun Fun. 2015. Fabrication And Characterization Of New PSF/PPSU UF Blend Membrane For Heavy Metal Rejection.

Desalination and Water Treatment. 1–10.

- [21] Urkiaga, A, Iturbe, D, Etxebarria, J. 2015. Effect Of Different Additives On The Fabrication Of Hydrophilic Polysulfone Ultrafiltration Membranes. *Desalination and Water Treatment*. 56(13): 3415– 3426
- [22] Sinha, M. K, Purkait, M. K.
 2014. Preparation And Characterization Of Stimuli-Responsive Hydrophilic Polysulfone Membrane Modified With Poly (N-Vinylcaprolactam-Co-Acrylic Acid). *Desalination*. 348(1): 16–25.
- [23] Yurekli, Y. 2016. Removal Of Heavy Metals In Wastewater By Using Zeolite Nano-Particles Impregnated Polysulfone Membranes. Journal of Hazardous Materials. 309: 53– 64.
- [24] Dong, L.-X, Yang, H.-W, Liu, S.-T,Wang, X.-M, Xie, Y. F. 2015. Fabrication And Anti-Biofouling Properties Of Alumina And Zeolite Nanoparticle Embedded Ultrafiltration Membranes. *Desalination*. 365: 70–78.
- [25] Liu, F, Ma, B.-R, Zhou, D, Xiang, Y.-H, Xue, L.-X. 2014. Breaking Through Tradeoff Of Polysulfone Ultrafiltration Membranes By Zeolite 4A. *Microporous and Mesoporous Materials*. 186: 113–120.
- [26] R. Kumar, A.M. Isloor, Α. Ismail. S. A. Rashid, T. Matsuura. 2013. Polysulfone-Chitosan Blend Ultrafiltration Membranes: Preparation, Characterization, Permeation And Antifouling Properties. RSC Adv. 3: 7855-7861.
- [27] AndriyYaroshchuk and Thomas Luxbacher. 2010. Interpretation

of Electrokinetic Measurements with Porous Films: Role of Electric Conductance and Streaming Current within Porous structure. *Langmuir*. 26(13): 10882–10889.

- [28] Song Zhaoa, Zhi Wanga, Xin Jixiao Wei, Boran Zhaoa, Wanga, Shangbao Yanga, Shichang Wang. 2011. Performance Improvement Of Polysulfone Ultrafiltration Membrane Using Panieb As Both Pore Forming Agent And Hydrophilic Modifier. Journal of Membrane Science. 385–386: 251-262.
- [29] Yaozu Liao, Thomas P. Farrell, Gregory R. Guillen, Minghua Li, James A. T. Temple, Xin-Gui Li, Eric M. V. Hoek and Richard B. Kaner. 2014. Highly Dispersible Polypyrrole Nanospheres For Advanced Nanocomposite Ultrafiltration Membranes. Mater. Horiz. 1: 58.
- [30] D. Rana, T. Matsuura. 2010. Surface Modifications for Antifouling Membranes, *Chem. Rev.* 110: 2448–2471.
- [31] Kimura K, Hane Y, Watanabe Y, Amy G, Ohkuma N. 2004. Irreversible Membrane Fouling During Ultrafiltration Of Surface Water. *Water Res.* 38: 3431–41.
- [32] V. Vatanpour, S. S. Madaeni, R. Moradian, S. Zinadini and B.

Astinchap. 2011. Fabrication And Characterization Of Novel Antifouling Nanofiltration Membrane Prepared From Oxidized Multiwalled Carbon Nanotube/Polyethersulfone Nanocomposite. J. Membr. Sci. 375: 284–294.

- [33] H. Zhao, L. Wu, Z. Zhou, L. Zhang and H. Chen. 2013. Improving The Antifouling Property Of Polysulfone Ultrafiltration Membrane Bv Incorporation Isocvanate-Of Treated Graphene Oxide, Phys. Chem. Chem. Phys. 15: 9084-9092.
- [34] M. Sun, Y. Su, C. Mu and Z. Jiang. 2009. Improved Antifouling Property of PES Ultrafiltration Membranes Using Additive of Silica–PVP Nanocomposite, Ind. *Eng. Chem. Res.* 49: 790–796.
- [35] A. Sotto, A. Boromand, S. Balta, J. Kim and B. van der Bruggen.
 2011. Doping Of Polyethersulfone Nanofiltration Membranes: Antifouling Effect Observed At Ultralow Concentrations Of TiO₂ Nanoparticles. J. Mater. Chem.
 21: 10311–10320.